Chnmer

## INTRODUCTION TO OPEN-END BELTS

Megadyne started manufacturing moulded transmission belts in 1957 and extruding open ended belts in 1975. Megalinear open length belts are manufactured in thermoplastic polyurethane, that gives superior wear and abrasion resistance. Various types of steel cord, offer good running characteristics, even under high tractive loads. Advanced production processes, allow the ability to engineer bespoke technical design solutions to meet market demands. By selecting from a range of components and materials, Megalinear belts can be manufactured to perform in even the most demanding applications. MEGALINEAR open-end belts are particularly suited where the most precise accuracy of position, low noise and long maintenance free cycles are the key requirements.

Megadyne has expanded the Megalinear range to include:

- MEGALINEAR QST
- MEGALINEAR GW
- MEGALINEAR FC - FCM - XMD
- MEGALINEAR MEGAC4T ${ }^{\text {™ }}$

Uniquely designed to reduce the noise levels, generated during high speed operations, MEGALINEAR QST is completely self-tracking without the need for flanged pulleys. The nylon faced helical offset teeth design, provides a high torque capacity.

For heavier applications, Megadyne have introduced the MEGALINEAR GW, a high performance thermoplastic polyurethane belt. Superior load capacities can be achieved due to the high shear strength of the tooth design, coupled with high tension, steel zinc coated cords, MEGALINEAR GW guarantees a greater transmittable power under continuous high loads.

MEGALINEAR FC is a new range of belts of the MEGALINEAR family. Specifically introduced for the food processing industry, MEGALINEAR FC is manufactured with Food Contact approved materials, according to European regulations EU 1935/2004, EU 10/2011 and EU 174/2015. It's manufactured in T5/T10 pitches without nose gap between the teeth and available with a variety of backing profiles, for all kinds of conveying and processing applications. These advanced FDA synchronous belts have excellent resistance to chemicals and corrosion, certified for wet and dry food contact. The homogenous belt design ensures a significantly greater service life, with a high level of hygienic integrity.

On request and with minimum quantity, it's possible to produce MEGALINEAR FCM, made in sky blue colour (RAL 5012) and certified for direct contact with dry and wet food.

Both MEGALINEAR FC AND FCM can be made with a special Metal and X-Ray detectable compound. MEGALINEAR XMD decreases the risk of contamination from belt fragments protecting Consumer Safety.



MEGAC4?
Megalinear Adaptable Cleats For Transport - is the most versatile belt ever! Its design with quick and easy interchangeable profiles means you can use the same belt for a wide variety of applications, transporting goods of different shapes on a single transport system with a minimum of downtime!

Thanks to their features, Megalinear belts can be successfully used in a wide range of applications such as:

- automatic sliding doors and garage opening system
- elevators
- automated handling devices
- linear drivers
- positioning system
- conveyors
- wood industry
- textile machine
- serigraphic industry
- glass industry
- stone and marble industry
- packaging industry
- robot systems
- tobacco industry
- paper and carton industry
- chemist and pharmaceutical industry
- Food industry

Megadyne has developed a very wide range of solutions with numerous tooth designs, tensile members and compound, suitable for all applications.

## STANDARD RANGE

MXL•XL•L•H•XH
T2,5•T5* • TT5 • T10* • T20

AT3 • AT5 • AT10 • MEGAC4T ${ }^{T M}$ AT10•AT20

MTD3 • MTD5 • MTD8 • MTD14

RPP5•RPP8•RPP14•RPP14XHP

STD5 • STD8

HG•TG5•TG10K6•TG10K13•TG20•ATG5•ATG10•ATG20

QST5 • QST8 • QST14

GW14 • GW20

[^0]
## CLASSIFICATIONS

Megalinear Timing Belts are manufactured in thermoplastic polyurethane, with single parallel steel cords. This type of belts, developed by our Research \& Development, offers good running characteristics and high traction loads. They are especially suited for power transmission and conveying with high loads and speeds. The addition of a nylon coating on the teeth during production enhances the running properties for specific applications and reduces the noise due to a lower frictional coefficient. An extra thickness of special coating is also possible on the back of the belt offering extra protection against aggressive or heavy products.

1. The body of the belts is white thermoplastic polyurethane 92 ShA, characterized by high levels of wear resistance even in the presence of shock and surge loading.
2. High strength $S$ and $Z$ parallel zinked steel tension members allow high breaking load and extremely low elongation. The combination of these high grade materials improves belt performances which can be summarised as follows:

- exceptional resistance to abrasion and tooth shear
- low coefficient of friction
- high flexibility
- ozone and temperature resistance $\left(-25^{\circ} \mathrm{C} /+80^{\circ} \mathrm{C}\right)$
- oil, grease and gasoline resistance



## MECHANICAL AND CHEMICAL CHARACTERISTICS

- Constant dimensions
- Noiseless
- Free maintenance
- High flexibility
- High resistance steel traction cords, with little stretching and top flexibility
- Linear speeds up to $20 \mathrm{~m} / \mathrm{s}$


## BODY

Megalinear belts are manufactured with white thermoplastic Polyurethane 92 ShA as standard.
Special compounds (different hardnesses, special properties) are available on request. Special compound and cords have to be tested and homologated on the application. Megadyne is not responsible for wrong functioning of special products. Here under some PU characteristics:

| Water | No problem in normal or sea clean water, at room temperature. |
| :---: | :---: |
|  | Over $60{ }^{\circ} \mathrm{C}$ there is a fast decrement of breaking strength. |
| Acids | In acid diluted proportions, at room temperature, this PU is moderately attacked. |
|  | In high concentration acid solutions, this PU has a very short lifespan. |
|  | Over $50^{\circ} \mathrm{C}$, acids are always dangerous for Thermoplastic PU. |
| Alkalis | In alkalis diluted proportions, at room temperature, this PU is moderately attacked. |
|  | In high concentration alkaline solutions, this PU has a very short lifespan. |
|  | Over $50{ }^{\circ} \mathrm{C}$, alkalis are always dangerous for Thermoplastic PU. |
| Solvents | Thermoplastic PU is insoluble in the greater part of solvents. |
|  | Only the very polar solvents (same as tetrahydrofuran, dimethylformamide, n-methylpyrrolidone) can dissolve or tight damage PU. |
|  | The Esters or the Ketons (same as ethyl acetate or methylethylketene) can usually produce a bulge, decreasing mechanical characteristics. |
|  | The Hydrocarbons aromatic and the Hydrocarbons aliphatic produce very high bulge. All the effects increase by increasing temperature. |
| Oils | PU has a high resistance to mineral pure oils (lubrificants, engine oils, combustible oils). |
|  | Usually, high performance syntetic oils, due to special additives contained, can be incompatible with Thermoplastic PU, especially at high temperature. |


| Greases | PU has a high resistance to mineral pure greases (lubrificants greases). |
| :---: | :---: |
|  | Usually, high performance syntetic greases, due to special additives contained, can be incompatible with Thermoplastic PU, especially at high temperature. |
| Fuels | Good resistance to petrols without Alcohols. |
|  | In presence of Alcohols, Thermoplastic PU can suffer deterioration. |
|  | Fuels including Aromatiche stuffs can produce reversible bulges. |
| Microorganisms | In presence of grime, containing humidity, Microorganisms can develop. |
|  | In case that Microbic attack can produce danger, you have to use a special kind of PU. |
| Weather agents | Good resistance to atmospheric agents. White colour can change to light yellow under long UV exposure. In any case this hasn't influence on mechanical resistance. |

## CORDS <br> Standard cord Kevlar

Megalinear is manufactured with $S$ and $Z$ parallel zinked steel cords as standard.
Kevlar tension cords are suggested for:

- Non magnetic, for use in drives with metal detectors
- Widely used in the food industry
- Applications in damp evoironement must be avoided

Kevlar cord belts have a lower dimentional stabiliy compared to stell cord belts. Length and tollerance may change.

## COATING

Megalinear can be manufactured with special coating on the teeth or on the back. Please check on page 120 and 121.

## IDENTIFICATION CODE

Using the information in the table below, it is possible to identify the correct belt for every application. The code is composed of letters and numbers as the following example::

| 1 |  | 2 |  | 3 |  | 4 |  | 5 |  | 6 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| J | + | 50 | + | AT | + | 10 | + | 10000 | + | SPECIAL MANUFACTURES |

1) J joined belt.

ML Megalinear belt open-end.
2) 50 this number indicates the width of requested belt. The value is in mm for a belt with a pitch in mm, and in inches for a belt with a pitch in inches.
3) AT this code composed by letters indicates the selection of profile.
4) 10 this number indicates the standard pitch of the belt. It is expressed in mm.
5) $\mathbf{1 0 0 0 0}$ the last number indicates the length of the belt always in mm regardless of pitch.
6) SPECIAL MANUFACTURES:

- special cords as Kevlar or HP or HF or HPF or stainless steel
- special compound as different hardness 85 ShA or different colours (black - red - yellow - blue)
- extra coating NFT or NFB or AVAFC or Tenax or Linatex or Honey comb or PU black cellulose or PU yellow or Neoprene rubber.


## LINEAR MOTION BELT



OMEGA LINEAR MOTION BELT


The following pages contain data, formulae and tables that are required to design a new belt drive.
For critical and difficult drives, it is raccomended that you contact our Application Department for advice.

| Symbol | Unit | Definition | Symbol | Unit | Definition |
| :---: | :---: | :---: | :---: | :---: | :---: |
| a | $\mathrm{m} / \mathrm{s}^{2}$ | acceleration | g | $\mathrm{m} / \mathrm{s}^{2}$ | gravity ( 9,81 ) |
| b | mm | belt width | $\boldsymbol{\mu}$ | - | friction coefficient |
| C | - | safety factor | m | Kg | conveyed mass |
| $\Delta \mathrm{l})_{00}$ | \% | elongation | $M_{\text {t }}$ | Nm | drive torque |
| d | mm | idler pitch diameters | n | 1/min | revs/min (RPM) of drive sprocket 1 |
| $\mathrm{d}_{1}$ | mm | sprocket pitch diameter | P | KW | drive power |
| $\mathrm{F}_{\mathrm{p}}$ | N | pretension | Q | N | force exerted by mass (m) |
| $\mathrm{F}_{\mathrm{u}}$ | N | peripheral force | V | $\mathrm{m} / \mathrm{s}$ | belt speed |
| $\mathrm{F}_{\mathrm{p} \text { spec }}$ | $\mathrm{N} / \mathrm{cm}$ | transmittable force per tooth per unit width | $z_{i}$ |  | number of teeth of sprocket |
| MTL | N | max traction load | $\mathrm{Z}_{\mathrm{m}}$ |  | number of teeth in mesh on driver sprocket (12) |
| BS | N | breaking strength | $\mathrm{Z}_{\mathrm{L}}$ |  | number of teeth of large pulley |
| c | mm | centre distance | $\mathrm{Z}_{\text {s }}$ |  | number of teeth of small pulley |
|  |  |  | p |  | belt pitch |

Max traction load is maximum acceptable traction on cords. Breaking strength is necessary load to break belt cords.
Elongation is belt elongation under load.

## USEFUL FORMULAE AND CONVERSION FACTORS

$$
\begin{array}{lll}
V=\frac{d_{1} \cdot n_{1}}{19100} & n_{1}=\frac{V \cdot 19100}{d_{1}} & d_{1}=\frac{V \cdot 19100}{n_{1}} \\
P=\frac{M_{t} \cdot n_{1}}{9550} & M_{t}=\frac{9550 \cdot P}{n_{1}} & M_{t}=\frac{F_{u} \cdot d_{1}}{2000}
\end{array} \quad Q=m \cdot g
$$

## CHOICE OF BELT PITCH AND SPROCKETS

For optimum belt pitch see tables on page 10.
For optimum choice of sprocket size, it is desiderable to have as near to 12 teeth in mesh as possible.


## BELT WIDTH AND PROFILE ESTIMATION

The belt width $b$ should be calculated using the following formula

$$
\begin{array}{lll}
\mathrm{b}=\left(\mathrm{F}_{\mathrm{u}} \cdot \mathrm{c}_{\mathrm{s}} \cdot 10\right) /\left(\mathrm{F}_{\mathrm{p} \text { spec }} \cdot \mathrm{Z}_{\mathrm{m}}\right) & \mathrm{C}_{\mathrm{s}} & =\text { safety factor from page } 11 \text { table } 4 \\
\mathrm{~F}_{\mathrm{u}} & =\text { from above calculation } \\
\mathrm{Z}_{\mathrm{m}} & =\text { number of teeth in mesh on driver sprocket } \\
\mathrm{Z}_{\mathrm{m}} & =\left[0,5-\frac{4 \cdot \mathrm{p}}{79 \cdot \mathrm{c}}\left(\mathrm{Z}_{\mathrm{L}}-\mathrm{Z}_{\mathrm{s}}\right)\right] \cdot \mathrm{Z}_{\mathrm{s}} \\
& & \left.=\text { (if calculated } Z_{\mathrm{m}}>=12 \text { for an open-end application use } \mathrm{Z}_{\mathrm{m}}=12\right) \\
& \left.=\text { (if calculated } \mathrm{Z}_{\mathrm{m}}>=6 \text { for a joined application use } Z_{m}=6\right) \\
\mathrm{F}_{\mathrm{p} \text { spec }} & =\text { transmittable force per tooth per unit width (see table on belt data pages) }
\end{array}
$$

## PRE-TENSIONING

The suggested installation tension:

$$
\begin{aligned}
& F_{p}=2 \cdot F_{u} \text { for linear and omega linear movement applications } \\
& F_{p}=F_{u} \text { for conveyor applications }
\end{aligned}
$$

## CORD CHECK

The maximum allowable tensile load of the belt pitch/width combination selected (see tables on belt data pages):


Ensure that all selected pulley and idler diameters are equal to or greater than the minimum values specified in corresponding belt data page.

## ELONGATION

When the belt is operating there will be an elongation proportional to max traction load:

$$
\Delta \mathrm{l} /{ }_{00}=\left(\mathrm{F}_{\mathrm{u}} \cdot 4\right) / \text { max traction load }
$$

## MACHINE DATA

$\mathrm{C}=2.000 \mathrm{~mm}$
$\mathrm{d}_{1}=76 \mathrm{~mm}$
$\mathrm{n}_{1}=300 \mathrm{RPM}$
$P=1,8 \mathrm{KW}$
low fluctuating load


## CHOICE OF BELT PITCH AND SPROCKETS

According to the belt pitch selection table $n .1$ on page 10 considering the values of $P$ and $n_{1}$, we select RPP8 belt.
Then we consider the pulley diameter nearest to the requested value and the corresponding n . of teeth (see technical information on page 65).
Therefore $Z_{1}=30$ teeth (with a pitch diameter of 76,4 mm).

## CALCULATION OF THE EFFECTIVE TENSION

Since the drive power is known, $\mathrm{F}_{\mathrm{u}}$ can be calculated

$$
F_{u}=\frac{19,1 \cdot 10^{6} \cdot P}{d_{1} \cdot n_{1}}=\frac{19,1 \cdot 10^{6} \cdot 1,8}{76,4 \cdot 300}=1500 \mathrm{~N}
$$

## DETERMINATION OF THE BELT WIDTH



Since the next closest width is $30 \mathrm{~mm}: 30$ RPP8 is choosen

## PRE-TENSIONING

$\mathrm{F}_{\mathrm{p}}=2 \cdot \mathrm{~F}_{\mathrm{u}} \quad \mathrm{F}_{\mathrm{p}}=3000 \mathrm{~N}$


## CORD CHECK

From page 64, RPP8 pitch 30 mm wide: max traction load 4750 N
max traction load $>\frac{F_{p}}{2}+\left(F_{u} \cdot C_{s}\right) \quad \frac{F_{p}}{2}+\left(F_{u} \cdot C_{s}\right)=1500+1500 \cdot 1,4$
$4750 \mathrm{~N}>3600 \mathrm{~N}$ selected belt is acceptable.

## SPROCKET AND IDLER DIAMETER CHECK

Ensure that all selected pulley and idler diameters are greater than or equal the minimum values specified on page 65.

## ELONGATION

$\Delta \mathrm{I}_{00}=\frac{\mathrm{F}_{\mathrm{u}} \cdot 4}{\text { max traction load }}=\frac{1500 \cdot 4}{4750}=1,26 \mathrm{~mm} / \mathrm{m}$
In the dynamic situations you will have an elongation of $1,26 \mathrm{~mm}$ per meter of operating belt.

## MACHINE DATA

$\mathrm{C}=5.000 \mathrm{~mm}$
$\mathrm{d}_{1}=100 \mathrm{~mm}$
$\mathrm{V}=0,5 \mathrm{~m} / \mathrm{s}$
$\mathrm{a}=0,5 \mathrm{~m} / \mathrm{s}^{2}$
Guide in nylon
$\mathrm{Q}=4500 \mathrm{~N}$
low fluctuating load


## CALCULATION OF THE EFFECTIVE TENSION

Since the mass is known, $\mathrm{F}_{\mathrm{u}}$ can be calculated
$\mathrm{F}_{\mathrm{u}}=(\mathrm{m} \cdot \mathrm{a})+(\mathrm{m} \cdot \mathrm{g} \cdot \mu) \quad$ value of $\mu$ according to table 3 on
page $11=0,35$
$\mathrm{F}_{\mathrm{u}}=(460 \cdot 0,5)+(460 \cdot 9,81 \cdot 0,35)=1810 \mathrm{~N}$
$m=Q / g=4500 / 9,81=460 \mathrm{~kg}$

## CHOICE OF BELT PITCH AND SPROCKETS

According to the belt selection table $n$. 2 on page 10, considering the values of $F_{u}$ (for joined belts enter double of calculated $F_{u}$ in table 2), we select $T 10$. Then we consider the pulley diameter nearest to the requested value and the corresponding n . of teeth (see technical information page 35). Therefore $\mathrm{Z}_{1}=32$ teeth (with a pitch diameter of 101,86 mm).

## DETERMINATION OF THE BELT WIDTH



Since the next closest width is $100 \mathrm{~mm}: 100 \mathrm{~T} 10$ is choosen.

PRE-TENSIONING
$F_{\mathrm{p}}=\mathrm{F}_{\mathrm{u}}$ so $\mathrm{F}_{\mathrm{p}}=1810 \mathrm{~N}$

## CORD CHECK

From page 34, T10 pitch 100 mm wide joined: max traction load 5415 N
max traction load $>\mathrm{F}_{\mathrm{p}}+\left(\mathrm{F}_{\mathrm{u}} \cdot \mathrm{C}_{\mathrm{s}}\right) \quad \mathrm{Fp}+\left(\mathrm{F}_{\mathrm{u}} \cdot \mathrm{C}_{\mathrm{s}}\right)=1810+(1810 \cdot 1,4)$
$5415 \mathrm{~N}>4344 \mathrm{~N}$ selected belt is acceptable.

## SPROCKET AND IDLER DIAMETER CHECK

Checking technical data on page 35 for pulley and idlers, it can be seen that the drive has acceptable pulley diameters.

## ELONGATION

$\Delta \mathrm{I} \mathrm{I}_{00}=\frac{\mathrm{F}_{\mathrm{u}} \cdot 4}{\mathrm{max} \text { traction load }}=\frac{1810 \cdot 4}{5415}=1,33 \mathrm{~mm} / \mathrm{m}$
In the dynamic situations you will have an elongation of $1,33 \mathrm{~mm}$ per meter of operating belt.

## CALCULATION PARAMETERS

## BELT PITCH SELECTION



Table n. 2

Average values valid for standard steel cord. After belt selection, please check belt resistance on belt data page.

Table n. 3 - Friction coefficient
Sliding friction on dry surface
Polyurethane / smooth steel
$\mu=0,5$
Polyurethane / rough steel
$\mu=0,7$
Polyurethane / abrasive steel
Polyurethane NFT / smooth steel
$\mu=0,9$

Polyurethane NFT / rough steel
Polyurethane NFT / abrasive steel
Polyurethane / nylon
$\mu=0,25$

Polyurethane NFT / nylon
$\mu=0,35$
$\mu=0,6$
$\mu=0,35$
Polyurethane / aluminium
$\mu=0,15$
Polyurethane NFT / aluminium
$\mu=0,8$

Rolling friction on dry surface

| Bearing | $\mu=0,015$ |
| :--- | :--- |
| Roller / PU Belt | $\mu=0,03 / 0,06$ |
| Bush | $\mu=0,15$ |

## Table n. 4 - Safety factor

The choice of the Safety factor's, depends on the operating conditions.


A major difficulty installing transmission belt is to achieve correct belt tension. Lifetime of support bearings and transmission belts and therefore reliability of the complete system largely depends on an optimally adjusted belt tension. Pretension is the force needed to put tension into the system to avoid the belt jumping on the pulleys as in the example below:

## Not correct belt installation



For a correct system installation, all applications with Megalinear belt can be summarised according following two sketches:

1) Linear and omega linear motion belt

$\mathrm{F}_{\mathrm{u}}=$ peripheral force (see calculation pag. 8/9)
$r=$ pulley radius

## PROCEDURE TO MEASURE

The procedure to measure the tension of the belt is to use a Belt Tension Gauging Equipement. This device consists of a small sensing head which is held across the belt to be measured. The belt is then tapped to induce the belt to vibrate at its natural frequency. The vibrations are detected and the frequency of vibration is then displayed on the measuring unit. The relation between belt static tension $\left(T_{s}\right)$ and frequency of vibration ( $f$ ) may be calculated using the following formula:


$$
f=\frac{1}{2 t} \cdot \sqrt{\frac{T_{s}}{m}} \quad \text { or } \quad T_{s}=4 \cdot m \cdot t^{2} \cdot f^{2}
$$

Where :

$$
\begin{array}{ll}
T_{S}=\text { static tension }(N) & f=\text { Frequency of vibration in Hertz }(\mathrm{Hz}) \\
m=\text { Belt mass per unit length }(\mathrm{kg} / \mathrm{m}) & t=\text { Free belt span length in meters }(\mathrm{m})
\end{array}
$$

For a correct system functioning and to increase belt life, it is necessary a correct pulley installation: pulleys has to be parallel and aligned as shown in drawing 1 (correct configuration).
If pulleys are not parallel as in drawing 2, belt could fall during functioning and this can provoke damages to complete equipment.
To grant a correct belt running, $\alpha$ and $\Delta x$ must be as smaller as possible. For more information, please contact our technical staff.


In omega application to grant good mesh between pulley and teeth and to respect belt flexibility avoiding excessive stress on cords, distance d (as drawing 4) has to be:
d $=4 \cdot$ belt width
Suggested angle $120^{\circ}$

Moreover for a good drive work, it is suggested to check belt straigthness as follows:


## FIXING PLATES

The fixing plates are used to fix the tail of the open belts.
On the customer's request, the plates can be delivered with or without fixing holes.
As the belt can't be stretched with the fixing plates we suggest to use other tension system.
The plates are delivered in aluminium alloy.
The Megadyne Technical Staff is ready to study special or particular applications.


XL - L - H - T5 - T10 - T20 - AT5 - AT10 - AT20
Order code example: AT10 pitch clamping plate for 25 mm width belt.


Clamping plates for imperial pitch belts


Clamping plates for HTD pitch belts
Belt width (mm)

| $\begin{aligned} & \underline{E} \\ & \frac{E}{E} \\ & \frac{1}{E} \\ & \frac{1}{4} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  | w | ( |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Pitch | F | d | B | A | S | 6 | 9 | 10 | 15 | 20 | 25 | 30 | 40 | 50 | 55 | 85 | 115 | 170 |
|  |  |  |  |  |  |  | C |  |  |  |  |  |  |  |  |  |  |  |  |
|  | - 5 M | 6 | 5,5 | 3,25 | 41,5 | 8 | 25 | 28 | - | 34 | - | 44 | - | - | - | - | - | - | - |
|  | - 8M | 8 | 9 | 5 | 66 | 15 | - | - | 35 | 40 | 45 | - | 55 | - | 75 | - | 110 | - | - |
|  | -14M | 10 | 11 | 9 | 116 | 22 | - | - | - | - | - | 56 | - | 71 | - | 86 | 116 | 146 | 201 |

Clamping plates for metric pitch belts
Belt width (mm)


[^1]



| $\begin{aligned} & \bar{\Phi} \\ & \stackrel{\otimes}{\omega} \end{aligned}$ | Clamping plates for GW20 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | BELT'S WIDTH (mm) | A (mm) | C (mm) | S (mm) | $\mathrm{F}(\mathrm{mm})$ | $\mathrm{d}(\mathrm{mm})$ | Screws UNI-EN 14399-8.8 | $N^{\circ}$ of svrews |
|  | Pitch | 50 | 340 | 110 | 36 | 15 | 16,5 | M16 | 2X3 |
|  | - GW20 | 100 | 340 | 160 | 36 | 15 | 16,5 | M16 | 2X3 |
|  |  | 150 | 340 | 210 | 36 | 15 | 16,5 | M16 | 2X4 |
|  |  | 200 | 340 | 260 | 36 | 15 | 16,5 | M16 | 2X5 |

Backlash between belt and pulley teeth is very important for positioning and transmission synchronism.


To imporve transmission precision, it is possible to use zero or reduced backlash pulleys. Please note that these pulleys don't reduce the elasticity of belt teeth or cords.

Maximum recommend pulley teeth is:


In following table there is a list of average values for backlashes:

| Available pitch for "zero" backlash pulley | T5 XL | T10 L H | T20 XH | AT5 | AT10 | AT20 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Average backlash value for standard | 0,6 | 1,2 | 2,4 | 0,2 | 0,4 | 0,8 |

RPP belts and pulleys offer great solution for positioning system because their parabolic profile reduces backlash and improves meshing quality.


XLLH


[^0]:    * Available in Food Contact (FC) / X-Ray and Metal detectable (XMD) versions.

[^1]:    - Available in customized length

